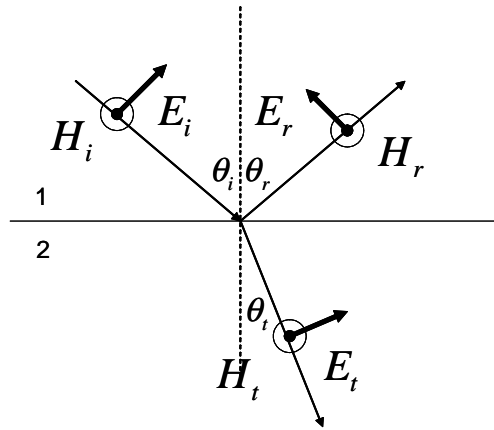


Chapter 9

Fresnel Reflection

9.0.1 π polarization:



We have from the law of reflection that

$$\theta_i = \theta_r \quad (9.1)$$

We have from Snell's law that

$$n_1 \sin \theta_i = n_2 \sin \theta_t \quad (9.2)$$

Boundary conditions for the tangential components of \mathbf{H} give us

$$H_i + H_r = H_t \quad (9.3)$$

or

$$\frac{E_i}{Z_1} + \frac{E_r}{Z_1} = \frac{E_t}{Z_2} \quad (9.4)$$

or

$$E_t = \frac{Z_2}{Z_1}(E_i + E_r)$$

and

$$E_i \cos \theta_i - E_r \cos \theta_r = E_t \cos \theta_t \quad (9.5)$$

and

$$E_i \cos \theta_i - E_r \cos \theta_i = \frac{Z_2}{Z_1}(E_i + E_r) \cos \theta_t \quad (9.6)$$

and defining

$$r = \frac{E_r}{E_i} \quad (9.7)$$

, we have

$$\cos \theta_i - r \cos \theta_i = \frac{Z_2}{Z_1}(1 + r) \cos \theta_t \quad (9.8)$$

and

$$\cos \theta_i - \frac{Z_2}{Z_1} \cos \theta_t = r(\cos \theta_i + \frac{Z_2}{Z_1} \cos \theta_t) \quad (9.9)$$

and finally

$$r = \frac{Z_1 \cos \theta_i - Z_2 \cos \theta_t}{Z_1 \cos \theta_i + Z_2 \cos \theta_t} \quad (9.10)$$

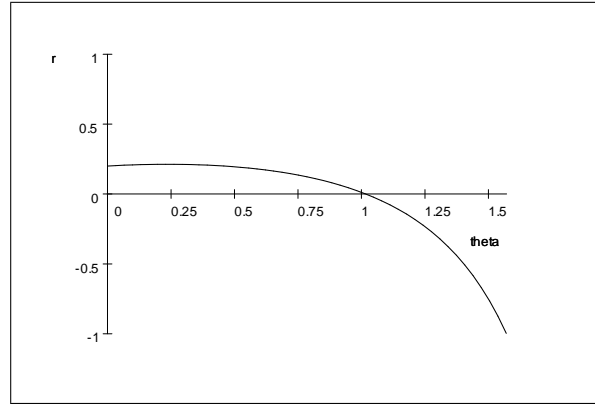
If the material is non-magnetic, then

$$r = \frac{n_2 \cos \theta_i - n_1 \cos \theta_t}{n_2 \cos \theta_i + n_1 \cos \theta_t} \quad (9.11)$$

and writing θ_t explicitly, we get

$$r = \frac{n_2 \cos \theta_i - n_1 \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_i}}{n_2 \cos \theta_i + n_1 \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_i}} \quad (9.12)$$

Plotting this for glass, with $n_1 = 1$, $n_2 = 1.5$, gives



We note that r goes to zero at the Brewster angle; here $\tan \theta_i = \frac{n_2}{n_1}$.

We also define the transmission coefficient

$$t = \frac{E_t}{E_i} \quad (9.13)$$

which, since

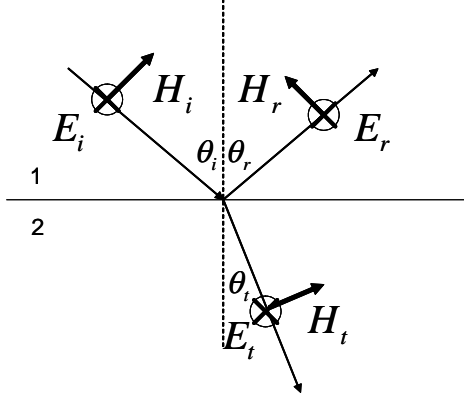
$$E_t = \frac{Z_2}{Z_1}(E_i + E_r) \quad (9.14)$$

becomes

$$t = \frac{Z_2}{Z_1}(1+r) = \frac{Z_2}{Z_1} \left(1 + \frac{Z_1 \cos \theta_i - Z_2 \cos \theta_t}{Z_1 \cos \theta_i + Z_2 \cos \theta_t}\right) = \frac{2Z_2 \cos \theta_i}{Z_1 \cos \theta_i + Z_2 \cos \theta_t} = \frac{2n_1 \cos \theta_i}{n_2 \cos \theta_i + n_1 \cos \theta_t} \quad (9.15)$$

9.0.2 σ Polarization

For σ polarization, we have



and here

$$E_i + E_r = E_t \quad (9.16)$$

or

$$\frac{H_i}{Z_1^{-1}} + \frac{H_r}{Z_1^{-1}} = \frac{H_t}{Z_2^{-1}} \quad (9.17)$$

or

$$H_t = \frac{Z_2^{-1}}{Z_1^{-1}}(H_i + H_r)$$

and

$$H_i \cos \theta_i - H_r \cos \theta_r = H_t \cos \theta_t \quad (9.18)$$

and

$$H_i \cos \theta_i - H_r \cos \theta_r = \frac{Z_2^{-1}}{Z_1^{-1}}(H_i + H_r) \cos \theta_t \quad (9.19)$$

and defining

$$r = \frac{E_r}{E_i} = \frac{H_r}{H_i} \quad (9.20)$$

, we have

$$\cos \theta_i - r \cos \theta_r = \frac{Z_2^{-1}}{Z_1^{-1}}(1 + r) \cos \theta_t \quad (9.21)$$

and

$$\cos \theta_i - \frac{Z_2^{-1}}{Z_1^{-1}} \cos \theta_t = r \left(\cos \theta_i + \frac{Z_2^{-1}}{Z_1^{-1}} \cos \theta_t \right) \quad (9.22)$$

and finally

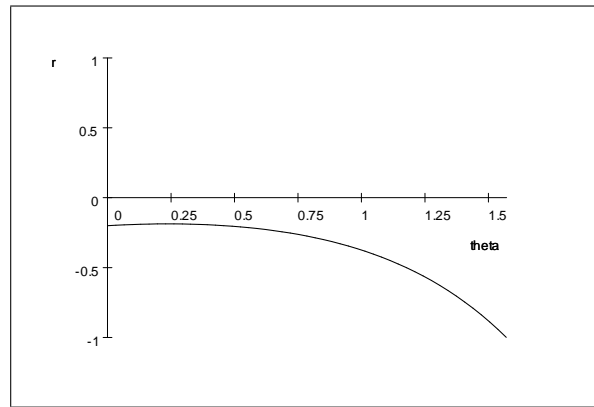
$$r = \frac{Z_2 \cos \theta_i - Z_1 \cos \theta_t}{Z_2 \cos \theta_i + Z_1 \cos \theta_t} \quad (9.23)$$

If the material is non-magnetic, then

$$r = \frac{n_1 \cos \theta_i - n_2 \cos \theta_t}{n_1 \cos \theta_i + n_2 \cos \theta_t} \quad (9.24)$$

and writing θ_t explicitly, we get

$$r = \frac{n_1 \cos \theta_i - n_2 \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_i}}{n_1 \cos \theta_i + n_2 \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_i}} \quad (9.25)$$



The transmittance is

$$t = \frac{E_t}{E_i} \quad (9.26)$$

and since

$$E_i + E_r = E_t \quad (9.27)$$

we have

$$\begin{aligned} t &= 1 + r = 1 + \frac{Z_2 \cos \theta_i - Z_1 \cos \theta_t}{Z_2 \cos \theta_i + Z_1 \cos \theta_t} = \frac{2Z_2 \cos \theta_i}{Z_2 \cos \theta_i + Z_1 \cos \theta_t} \\ &= \frac{2n_1 \cos \theta_i}{n_1 \cos \theta_i + n_2 \cos \theta_t} \end{aligned}$$

Summary

At an interface between two materials, we have, for π polarization

$$r_{12}^{\pi} = \frac{n_2 \cos \theta_1 - n_1 \cos \theta_2}{n_2 \cos \theta_1 + n_1 \cos \theta_2} \quad (9.28)$$

and

$$t_{12}^{\pi} = \frac{2n_1 \cos \theta_1}{n_2 \cos \theta_1 + n_1 \cos \theta_2} \quad (9.29)$$

while for σ polarization, we have

$$r_{12}^{\sigma} = \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2} \quad (9.30)$$

and

$$t_{12}^{\sigma} = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + n_2 \cos \theta_2} \quad (9.31)$$

9.0.3 Total Internal Reflection (TIR)

σ polarization

Consider the reflection coefficient for σ polarization.

$$r_{12}^{\sigma} = \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2} \quad (9.32)$$

Using Snell's Law, we can write

$$\sin \theta_2 = \frac{n_1}{n_2} \sin \theta_1$$

$$\cos \theta_2 = \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_1} \quad (9.33)$$

$$r_{12}^{\sigma} = \frac{n_1 \cos \theta_1 - n_2 \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_1}}{n_1 \cos \theta_1 + n_2 \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_1}} \quad (9.34)$$

Now suppose that $n_1 > n_2$. In this case, if

$$\sin \theta_1 > \frac{n_2}{n_1} \quad (9.35)$$

we have

$$\cos \theta_2 = i \sqrt{\frac{n_1^2}{n_2^2} \sin^2 \theta_1 - 1} \quad (9.36)$$

and $\cos \theta_2$ is imaginary (but $\sin \theta_t$ remains real), and r_{12}^σ is complex. It is useful to define the critical angle for TIR as

$$\sin \theta_c = \frac{n_2}{n_1} \quad (9.37)$$

or

$$\theta_c = \sin^{-1} \frac{n_2}{n_1} \quad (9.38)$$

Now we can write

$$r_{12}^\sigma = \frac{n_1 \cos \theta_1 - n_2 i \sqrt{\frac{n_1^2}{n_2^2} \sin^2 \theta_1 - 1}}{n_1 \cos \theta_1 + n_2 i \sqrt{\frac{n_1^2}{n_2^2} \sin^2 \theta_1 - 1}} = \frac{a - ib}{a + ib} \quad (9.39)$$

or

$$r_{12}^\sigma = |r_{12}^\sigma| e^{i\phi} \quad (9.40)$$

We write

$$r_{12}^\sigma = \frac{a - ib}{a + ib} \quad (9.41)$$

and note that

$$|r_{12}^\sigma| = \sqrt{r_{12}^\sigma r_{12}^{\sigma*}} = 1 \quad (9.42)$$

So the magnitude of the reflection coefficient is 1. Writing

$$r_{12}^\sigma = \frac{a - ib}{a + ib} = \frac{(a - ib)^2}{a^2 + b^2} = \frac{a^2 - b^2}{a^2 + b^2} - \frac{2iab}{a^2 + b^2} \quad (9.43)$$

the phase ϕ can be conveniently written as

$$\tan \phi = -\frac{2ab}{a^2 - b^2} = -\frac{2n_1 \cos \theta_1 n_2 \sqrt{\frac{n_1^2}{n_2^2} \sin^2 \theta_1 - 1}}{n_1^2 \cos^2 \theta_1 - n_2^2 \left(\frac{n_1^2}{n_2^2} \sin^2 \theta_1 - 1\right)} = -\frac{2n_1 \cos \theta_1 \sqrt{n_1^2 \sin^2 \theta_1 - n_2^2}}{n_1^2 (\cos^2 \theta_1 - \sin^2 \theta_1) + n_2^2}$$

The reflected wave has the same amplitude as the incident wave, but there is an angle-dependent phase shift. The reflection coefficient for the intensity is

$$R^\sigma = r_{12}^\sigma r_{12}^{\sigma*} = 1 \quad (9.44)$$

All of the incident power is reflected - this is total internal reflection. No power is transmitted.

The transmission coefficient is

$$t_{12}^{\sigma} = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + n_2 \cos \theta_2} = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + n_2 i \sqrt{\frac{n_1^2}{n_2^2} \sin^2 \theta_1 - 1}} \quad (9.45)$$

a complex number, which equals 2 at the critical angle of incidence θ_c .

It is interesting to look at the wavevector \mathbf{k}_2 . From Maxwell's equations we have (assuming isotropy and nonmagnetic materials) that

$$k_2^2 = \omega^2 \mu_o \varepsilon \quad (9.46)$$

or

$$k_2 = \frac{\omega n_2}{c} \quad (9.47)$$

The in-plane component of \mathbf{k}_2 (in the interface)

$$k_{2x} = k_2 \sin \theta_2 = k_1 \sin \theta_1 \quad (9.48)$$

and, since $\sin \theta_2$ is real, the in-plane component of the wave-vector \mathbf{k}_2 is real. Furthermore, θ_2 is such that Snell's law is satisfied;

$$k_2 \sin \theta_2 = k_1 \sin \theta_1 \quad (9.49)$$

We also have for the normal component k_{2z} of \mathbf{k}_2 that

$$k_{2z} = k_2 \cos \theta_2 \quad (9.50)$$

but this is imaginary, since

$$k_{2z} = k_2 i \sqrt{\frac{n_1^2}{n_2^2} \sin^2 \theta_1 - 1} \quad (9.51)$$

so we have an imaginary normal component of the wave vector. We can also write this as

$$k_{2z} = i \frac{n_1}{n_2} k_2 \sqrt{\sin^2 \theta_1 - \sin^2 \theta_c} = i k_1 \sqrt{\sin^2 \theta_1 - \sin^2 \theta_c}$$

In essence, what happens is the following. As the angle of incidence θ_1 increases, the angle of transmission θ_2 grows. At the critical angle, when

$\theta_1 = \theta_c$, \mathbf{k}_2 is in the plane of the interface. As the angle of incidence increases further, an imaginary component of \mathbf{k}_2 appears, normal to the interface. This increases the length of \mathbf{k}_2 sufficiently so that its projection on the interface can match that of the incident wave.

Note that

$$k_2^2 = \mathbf{k}_2 \cdot \mathbf{k}_2 = k_{2x}^2 - |k_{2z}^2|^2 \quad (9.52)$$

So, indeed, having an imaginary component allows k_2 to be longer. Substitution gives

$$k_1^2 \sin^2 \theta_1 - k_2^2 \left(\frac{n_1^2}{n_2^2} \sin^2 \theta_1 - 1 \right) = k_2^2 = \frac{\omega n_2}{c} \quad (9.53)$$

as expected.

The transmitted electric field at the interface is

$$\mathbf{E}_t = \mathbf{E}_i t_{12} \quad (9.54)$$

so it is just the incident field multiplied by a complex amplitude. Explicitly, we have

$$\mathbf{E}_t = E_{ot} \hat{\mathbf{y}} e^{i(\mathbf{k}_2 \cdot \mathbf{r} - \omega t)} = E_{ot} \hat{\mathbf{y}} e^{-k_{2z} z} e^{i(k_{2x} x - \omega t)} \quad (9.55)$$

so we have a real wave propagating along the interface, with wave vector

$$k_{2x} = k_2 \sin \theta_2 = k_1 \sin \theta_1 \quad (9.56)$$

and an exponentially decaying envelope normal to the interface with decay length

$$\zeta = \frac{1}{k_{2z}} = \frac{1}{k_1 \sqrt{\sin^2 \theta_1 - \sin^2 \theta_c}} = \frac{\lambda_o}{2\pi n_1 \sqrt{\sin^2 \theta_1 - \sin^2 \theta_c}} \quad (9.57)$$

The \mathbf{H} field is given, as usual, by

$$\mathbf{H}_t = \frac{1}{\omega \mu_o} \mathbf{k}_2 \times \mathbf{E}_t \quad (9.58)$$

or

$$\mathbf{H}_t = \frac{1}{Z_2} \hat{\mathbf{k}}_2 \times \mathbf{E}_t \quad (9.59)$$

and

$$\mathbf{H}_t = \frac{1}{Z_2} (\sin \theta_2 \hat{\mathbf{x}} + \cos \theta_2 \hat{\mathbf{z}}) \times E_t \hat{\mathbf{y}} = \frac{1}{Z_2} E_t \sin \theta_2 \hat{\mathbf{z}} - \frac{1}{Z_2} E_t \cos \theta_2 \hat{\mathbf{x}} \quad (9.60)$$

so \mathbf{H}_t has a real component along the z -direction, and an imaginary component along the x direction.

Is this still a transverse wave?

Is the relation

$$\nabla \cdot \mathbf{H} = \mathbf{k}_2 \cdot \mathbf{H}_t = 0 \quad (9.61)$$

satisfied? Substitution gives

$$\mathbf{k}_2 \cdot \mathbf{H}_t = \left(\frac{1}{Z_2} E_t \sin \theta_2 \hat{\mathbf{z}} - \frac{1}{Z_2} E_t \cos \theta_2 \hat{\mathbf{x}} \right) \cdot (k_2 \cos \theta_2 \hat{\mathbf{z}} + k_2 \sin \theta_2 \hat{\mathbf{x}}) = 0 \quad (9.62)$$

so although there are components of \mathbf{H}_t along the wavevector \mathbf{k}_2 , the dot product is zero.

Power is propagating along the interface, but no power propagates along the z -direction. This is because $\cos \theta_t$ is imaginary, and the average power propagating in the z -direction will have a time dependence of the form $\cos \omega t \sin \omega t$, whose time average is zero.

9.0.4 π polarization

Note that here the situation is the same as for σ polarization, except \mathbf{H} plays the role of \mathbf{E} , and vice versa.